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Thermal Radiation and Heat Absorption Effect on Heat and Mass Transfer over an Exponential Stretching Porous Surface with Viscous Dissipation

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Authors' contributions

This work was carried out in collaboration between all authors. Author OAE formulated the problem and the derivation of equations, author JFB solved the problem, did the table and the graphs. Author TOO carried out the mathematical analysis and discussion of result while author OEE managed the literature searches and review. All authors read and approved the final manuscript.

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ABSTRACT

The study of natural convective boundary layer flow of heat and mass transfer of incompressible viscous dissipative fluid over a porous stretching vertical surface in the presence of thermal radiation with heat absorption in a porous medium is considered. A similarity variables is used to reduce the governing system of PDEs to a set of nonlinear ordinary differential equations which are solved numerically using shooting technique coupled with fourth order Runge-Kutta method. The numerical computations are presented in graphically and tabular for various fluid parameters controlling the fluid flow of heat and mass transfer. It is observed that an increase in radiation produced a rise in the velocity, temperature and concentration profiles. Skin friction and Nusselt number increased with an increase in the radiation.

Keywords: Radiation; stretching surface; porosity; heat absorption; dissipation.

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1. INTRODUCTION

The study of compressible, laminar boundary layer flow of momentum, energy and species transfer over a stretching sheet are important from practical and theoretical point of view as a result of their wider applications in polymer technology and metallurgy. The thermal buoyancy forces arising due to the heating and flow species of stretching surface, under some circumstances, may alter significantly the flow, thermal and mass fields as well as the heat and mass transfer behaviour in the manufactuing processes [1-5]. As a result, [6] investigated the effects of radiation and heat source/sink on unsteady MHD boundary layer flow and heat
transfer over a shrinking sheet with transfer over a shrinking sheet with suction/injection. A study was carried out on the numerical solution for thermal radiation effect on inclined magnetic field of MHD free convective heat transfer dissipative fluid flow past a moving vertical porous plate with variable suction as in [7-10]. In the same vein, [11] investigated series solutions of unsteady magnetohydrodynamics flows of non-Newtonian fluids caused by an impulsively stretching plate. It was found out that for a fixed time with increasing Schmidt number, the concentration profiles reduces for fixed Schmidt number as time increases.

More also, [4] examined the influence of radiation and magnetic field effect on unsteady mixed convection flow over a vertical stretching/shrinking surface with suction/injection. The finding revealed that an increase in magnetic field parameter cause a decrease in the field flow rate. [12] presented the effect of heat generation and thermal radiation on MHD flow near a stagnation point on a linear stretching sheet in porous medium and presence of variable thermal conductivity and mass transfer. The analysis shows that an increase in the Prandtl number leads to a decrease in the temperature profile, while a rise in the thermal or solutant Grasshof number leads to increase in the velocity profile. [13] reported on nonlinear thermal radiation and chemical reaction effects on MHD 3D Casson fluid flow in porous medium. Fluid viscosity is assumed to vary as a linear function of temperature. Also, [8] investigated analytic solution for axi-symmetric flow and heat transfer of a second grade fluid past a stretching sheet.

Moreover, several literature are presented on boundary layer flow over a stretching plate where the velocity of the stretching surface is assumed to be linearly proportional to the distance from the fixed origin. However, [14] established that stretching of plastic sheet may not necessarily be linear. [15] examined the heat and mass transfer in the boundary layers on an exponentially stretching surface. Suction and heat transfer characteristics in the flow over an exponentially stretching sheet was presented by [16]. Approximate analytic similarity solution for viscoelastic boundary layer flow over an exponentially stretching surface has been investigated by [17]. While, [18,19] studied the effects of thermal radiation on the flow due to an exponentially stretching surface. MHD boundary layer flow due to an exponentially stretching sheet with radiation effect was studied by [20,21]. An analysis on the effect of magnetic field on boundary layer flow and heat transfer of a dusty fluid over an exponentially stretching surface with an exponential temperature distribution was reported by [22,23] they considering the Saffman model for flow problem. From the results, it was obtained that the effect of pressure variations within the enclosed space has a negligible effect on the buoyancy and on the resulting surface of the heat transfer coefficients.

This present study examine the combine effects of thermal radiation and viscous dissipation on heat and mass transfer over an exponentially porous stretching surface with heat absorption in a porous medium. The study is implemented using Runge-Kutta method with shooting techniques. The system remains invariant due to some relations among the parameters of the transformations. In section 2, the introduction to the study is presented, while section 3 illustrated the numerical solution and section 4 depicted the results and discussion of all important embedded parameters in the flow.

2. FLOW MODEL FORMULATION

Considering a free convective, the boundary layer flow, heat and mass transfer of viscous incompressible fluid over an exponentially stretching surface. The flow is produced as a result of linear stretching of the surface, caused by the simultaneous action of two forces along the *x* -axis. Keeping the origin fixed, the plate is stretched with a velocity $U_{\scriptscriptstyle 0}$, varying linearly with the distance from the slit. It is assumed that the stretching surface is kept at temperature T_w and the concentration C_w respectively. The ambient values are attained as $y \rightarrow \infty$, of *T* and *C* are

represented by *T*[∞] and *C*[∞] respectively. Under the usual boundary layer approximations, The geometry and equations governing the fluid flow of heat and mass transfer according to Boussinesq model [9,17,22], are as follows:

Fig. 1. The physical model and Coordinate System

$$
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0\tag{1}
$$

$$
u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = v\frac{\partial^2 u}{\partial y^2} + g\beta_\text{r}(T - T_\infty) + g\beta_\text{c}(C - C_\infty) - \frac{v}{K}u\tag{2}
$$

$$
\rho C_p \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) = k \frac{\partial^2 T}{\partial y^2} - \frac{\partial q_r}{\partial y} + \mu \left(\frac{\partial u}{\partial y} \right) - Q_0 (T - T_\infty)
$$
\n(3)

$$
u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} = D\frac{\partial^2 C}{\partial y^2} - \gamma(C - C_{\infty})
$$
 (4)

Subject to the following boundary conditions:

$$
u = U_0 e^{\frac{x}{L}}, v = -V_0 e^{\frac{x}{L}}, T = T_w = T_{\infty} + T_0 e^{\frac{x}{2L}}, C
$$

= $C_w = C_{\infty} + C_0 e^{\frac{x}{2L}}$ at $y = 0$
 $u \to 0, T \to T_{\infty}, C \to C_{\infty}$ as $y \to \infty$ (5)

where u , u , C , and T are velocity component in the *x* direction, velocity component in the *y* direction, concentration of the fluid species, fluid temperature respectively. *L* is the reference length, \boldsymbol{U}_0 is the reference velocity, \boldsymbol{V}_0 is the permeability of the porous surface respectively.

The physical quantities ρ , V , D , k , C_p , K , \mathcal{Q}_0 and γ are the density, fluid kinematics viscosity, coefficient of mass diffusivity, thermal conductivity of the fluid and specific heat, Porosity, heat absorption and reaction rate coefficient respectively. *g* is the gravitational acceleration, $\beta_{\scriptscriptstyle T}$ and $\beta_{\scriptscriptstyle C}$ are the thermal and mass expansion coefficients respectively. q_r is the radiative heat flux in the *y* direction. The Rosseland approximation is adopted for the expression of thick radiation heat flux in the heat equation with gray radiating liquid, non-scattering but with absorbing-emitting depending on wavelength [24,25]. The radiative heat flux q_r is given by

$$
q_r = -\frac{4\sigma_0}{3\delta} \frac{\partial T^4}{\partial y} \tag{6}
$$

where $\sigma_{\!_0}$ and δ are the Stefan-Boltzmann and the mean absorption coefficient respectively. Assume the temperature difference within the flow are sufficiently small such that $T^{\, 4}$ may be expressed as a linear function of temperature, using Taylor series to expand T^4 about the free stream $T_{\scriptscriptstyle{\infty}}$ and neglecting higher order terms, this gives the approximation.

$$
T^4 \cong 4T^3 T - 3T^4 \tag{7}
$$

In order to transform the governing equations (1) to (5), the following similarity transformations variables are introduced [17].

$$
\psi(x, y) = \sqrt{2vU_0L}e^{\frac{x}{2L}}f(\eta), \eta = y\sqrt{\frac{U_0}{2vL}}e^{\frac{x}{2L}}, T
$$

= $T_{\infty} + T_0e^{\frac{x}{2L}}\theta(\eta),$

$$
C = C_{\infty} + C_0e^{\frac{x}{2L}}\phi(\eta)
$$
 (8)

The governing equations reduces to system of ordinary differential equations as follow:

$$
f^{''} + ff^{'} - 2f^{2} + Gr\theta + Gc\phi - Daf^{'} = 0 \quad (9)
$$

$$
\left(1+\frac{4}{3}R\right)\theta^{2}+P_{r}f\theta^{3}-P_{r}f^{3}\theta+PrEc(f^{2})^{2}-PrQ\theta=0
$$
\n(10)

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$$
\phi^{'} + S_c f \phi^{'} - S_c f^{'} \phi - Sc \lambda \phi = 0 \tag{11}
$$

The corresponding boundary conditions take the form:

$$
f = f_w, f' = 1, \theta = 1, \phi = 1 \text{ at } \eta = 0
$$

$$
f' = 0, \theta = 0, \phi = 0 \text{ as } \eta \to \infty
$$
 (12)

where $Da = \frac{2\pi E}{\sigma} e^{-L}$ *x e* U_0K $Da = \frac{2\nu L}{\mu}e^{-\frac{2\nu L}{\mu}}$ 0 $=\frac{2V}{2V}e^{-\frac{x}{L}}$ is the Darcy parameter,

$$
Gr = \frac{2Lg\beta_T T_0}{U_0^2}e^{-\frac{3x}{2L}}
$$
 is the thermal Grashof

number, $Gc = \frac{2LgpcC_0}{\epsilon^2}e^{-2L}$ *x* $\frac{c}{c}$ ^o e *U* $Gc = \frac{2Lg\beta_cC_0}{r^2}e^{-\frac{3}{2}}$ 3 2 $\mathbf{0}$ $=\frac{2Lg\beta_cC_0}{\sigma^2}e^{-\frac{3x}{2L}}$ is the solutant

Grashof number, $Pr = \frac{P}{k}$ *C* $Pr = \frac{\rho V C_p}{I}$ is the Prandtl

number,
$$
Q = \frac{2LQ_0}{U_0 \rho C_p} e^{-\frac{x}{L}}
$$
 is the heat absorption

parameter, $R = \frac{1800}{\delta k}$ $R = \frac{4\sigma_0 T_s}{\delta k}$ $=\frac{4\sigma_0 T_{\infty}^3}{2}$ is the thermal radiation

parameter, $Sc = \frac{P}{D}$ $Sc = \frac{V}{R}$ is the Schmidt number,

$$
f_w = V_0 \sqrt{\frac{2L}{vU_0}} e^{-\frac{3x}{2L}}
$$
 is the permeability of the

plate, $\lambda = \frac{2L}{\mu}e^{-L}$ *x e U L* [−] 0 $\lambda = \frac{2L\gamma}{\sigma^2}e^{-\frac{x}{L}}$ is the chemical reaction

parameter, $Ec = \frac{c_0}{\rho(T-T^{\infty})}$ $=\frac{0}{\sqrt{2}}$ *T* −*T*∞ $Ec = \frac{U}{\sqrt{T}}$ ρ is the viscous dissipation parameter.

The skin friction coefficient C_{fix} , the Nusselt number Nu_{x} and the Sherwood Sh_{x} number are given by

$$
C_{fx} = \frac{2\mu}{\rho u_w^2} \frac{\partial u}{\partial y}\bigg|_{y=0} = \sqrt{\frac{2x}{LRe_x}} f'(0) \tag{13}
$$

$$
Nu_x = -\frac{x}{T_w - T_w} \frac{\partial T}{\partial y}\Big|_{y=0} = -\sqrt{\frac{xRe_x}{2L}} theta'(0) (14)
$$

$$
Sh_x = -\frac{x}{C_w - C_w} \frac{\partial C}{\partial y}\Big|_{y=0} = -\sqrt{\frac{xRe_x}{2L}} phi'(0) \quad (15)
$$

3. METHOD OF SOLUTION

The governing equations of convection, heat and mass transfer in fluids are essentially nonlinear ordinary differential equations. Hence, the system of nonlinear ordinary differential equations together with the boundary conditions are solved numerically using fourth order Runge-Kutta scheme with a shooting technique see [25,26].

$$
\mathsf{Let},
$$

$$
\begin{pmatrix}\n x_1 \\
 x_2 \\
 x_3 \\
 x_4 \\
 x_5 \\
 x_6 \\
 x_7 \\
 x_8 \\
 x_8 \\
 x_9\n\end{pmatrix}\n=\n\begin{pmatrix}\n \eta \\
 f \\
 f \\
 \eta \\
 \eta \\
 \theta \\
 \phi \\
 \phi \\
 \phi \\
 \phi\n\end{pmatrix}
$$
\n(16)

Then, it becomes,

$$
\begin{pmatrix}\nx_1 \\
x_2 \\
x_3 \\
x_4 \\
x_5 \\
x_6 \\
x_7 \\
x_8 \\
x_9 \\
x_9\n\end{pmatrix}\n\begin{pmatrix}\n1 \\
x_3 \\
x_4 \\
x_5 \\
x_7 \\
x_8 \\
x_9 \\
\end{pmatrix}\n\begin{pmatrix}\n1 \\
x_3 \\
x_4 \\
x_5 \\
x_7 \\
x_8 \\
x_9 \\
\end{pmatrix}\n\begin{pmatrix}\n17 \\
x_2 \\
x_3 + x_2x_4 - 2x_3^2 + Grx_6 + Gcx_8 - Dax_3 \\
x_7 \\
x_8 \\
x_9 \\
\end{pmatrix}\n\begin{pmatrix}\n17 \\
x_2 \\
x_3 \\
x_4 \\
x_5 \\
\end{pmatrix}\n\begin{pmatrix}\n18 \\
x_1 \\
x_2 \\
x_3 \\
\end{pmatrix}\n\begin{pmatrix}\n19 \\
x_2 \\
x_3 \\
x_4 \\
\end{pmatrix}\n\begin{pmatrix}\n19 \\
x_1 \\
x_2 \\
x_3 \\
\end{pmatrix}\n\begin{pmatrix}\n19 \\
x_2 \\
x_3 \\
\end{pmatrix}\n\begin{pmatrix}\n19 \\
x_1 \\
x_2 \\
x_3 \\
\end{pmatrix}\n\begin{pmatrix}\n19
$$

P	values	(0)	$\theta(0)$	$\phi(0)$	\boldsymbol{P}	values	(0)	$\theta(0)$	$\phi(0)$
$f_{\scriptscriptstyle{w}}$	0.5	-0.39356	-2.94639	-1.33911	$\mathbf C$ ມ	0.2	-0.38511	-3.94712	-0.75191
	1.0	-0.72229	-3.81430	-1.51023		0.62	-0.72229	-3.81430	-1.51023
	1.5	-1.11098	-4.77441	-1.70001		1.2	-0.92066	-3.73435	-2.35701
	2.0	-1.54965	-5.79574	-1.90816		2.0	-1.05491	-3.68497	-3.39680
Da	0.01	-0.68253	-3.82420	-1.51312	D	0.7	0.35638	-1.36411	-1.54371
	0.5	-0.88962	-3.77138	-1.49830		1.5	-0.56375	-2.29442	-1.52252
	1.0	-1.08057	-3.72021	-1.48521		3.0	-0.72229	-3.81430	-1.51023
	1.5	-1.25528	-3.67160	-1.47372		5.0	-0.81614	-5.68088	-1.50489

Table 1. Effect of $\,f_{_W},\,G_{_r},\,G_{_c},\,S_{_c},\,P_{_r},\,R\,$ and $\,\lambda\,$ on $\,f^{^{\,\prime}}(0),\,\theta^{^{\cdot}}(0)\,$ and $\,\phi^{^{\cdot}}(0)\,$

where $f_w, b_1, a_1, a_2, a_3, a_4$ are unknown constants to be determined.

The computations have been performed using a symbolic program and computational computer language MAPLE software.

From the process of numerical computation, the skin-friction coefficient, the local Nusselt number and the local Sherwood number, which are respectively proportional to $f^{'}(0)$, $\theta^{'}(0)$ and $\phi(0)$, at the plate have been examined for different values of the parameters are presented in a tabular form and discussed. The following parameter values are adopted for computation as default number: *Sc* = 0.62, *Pr* = 3, *Da* = 0.01 , $R = 0.1$, $\lambda = 1$, $fw = 1$, $Gr = 2$, $Gc = 2$, $Q = 0.5$, $Ec = 0.2$. All graphs are correspond to the value except otherwise indicated on the graph.

4. RESULTS AND DISCUSSION

Table 1 represent the numerical results of variation in Skin friction, Nusselt and Sherwood numbers at the surface with f_w , Da , S_c and

Pr which are of physical and engineering interest. From the results it seen that an increase in f_{w} decreases the skin friction, Nusselt and Sherwood numbers respectively due to decrease in the boundary layers. An increase in the values of *Da* decreases the skin friction but increases the Nusselt and Sherwood profiles. Variations in the value of S_c decreases the wall layer of skin friction and Sherwood number but increase the Nusselt number. Also, increase in *P^r* decreases the skin friction and Nusselt number while it causes increase in the Sherwood number.

Fig. 2 shows the effect of thermal Grashof number *Gr* on the rate of fluid flow. From the figure, it is seen that increasing in the parameter *Gr* leads to an increase in the flow rate, as a result, the velocity boundary layer thickened. Hence, heat as a strong influence on flow rate. While, the effect of solutant Grashof number *Gc* on the velocity distribution is illustrated in Fig. 3. It is noticed from the figure that the velocity increases with an increase in the values of the parameter *Gc* due to the fact that *Gc* increases free convection current and thereby increases the velocity distribution.

For variation in the values of radiation parameter *R* , the dimensionless velocity and temperature profiles are plotted in Figs. 3 and 4. It is obvious from the distribution that velocity and temperature increases with an increase in the radiation parameter. The effects is as a result of thickness in the momentum and thermal boundary layers. Figure 5 shows the velocity profiles for various values of the viscous dissipation parameter, Eckert number *Ec* . The Eckert number represent the relationship between the kinetic energy in the flow and the enthalpy. It contains the conservation of kinetic energy into internal energy by work done against the viscous fluid stress. Hence, it is found that as parameter *Ec* increases, the velocity distribution increases due to decrease in the fluid particle bounding forces.

Fig. 3. Velocity Profiles for different values of

injection parameter on the dimensionless velocity profiles. It is shown from figure that the suction parameter causes decrease in the velocity indicating the fact that suction stabilizes the boundary layer development, while the injection increases the velocity at the boundary layer indicating that injection supports the flow to penetrate more into the fluid. This is due to the fact that larger suction leads to faster cooling of the plate surface thereby decreases the flow fluid rate in the system.

Fig. 4. Temperature Profiles for different values of *R*

Fig. 5. Velocity Profiles for different values of *Ec*

The influences of the Prandtl number P_r on the temperature distribution are presented in Fig. 7. It can be noticed from the figure that as the Prandtl number P_r increases, the dimensionless temperature decreases, this is because, as the Prandtl number increases the thickness of the thermal boundary layer decreases and heat is able to diffuse out of the system, hence the temperature profiles decreases.

Fig. 8 depicts the behavior of Schmidt number *Sc* on the concentration profiles. Schmidt number can be define as the ratio of the momentum to the mass diffusivity. It is seen that the concentration profiles reduces as the

Schmidt number increases. Schmidt number quantifies the relative effectiveness of momentum and mass transport by diffusion in the hydrodynamic concentration boundary layers.

Fig. 6. Velocity Profiles for different values of

Fig. 7. Temperature Profiles for different values of *Pr*

Fig. 9 illustrates the effect of the porosity parameter *Da* on the velocity profiles. There are great changes that occur in the momentum boundary layers when changes are made to the values of porosity parameter. The velocity is decreased with an increase in the porosity parameter. Porosity resist free flow of fluid in the system.

The effects of the presence of heat sink *Q* on the temperature distribution is presented in figure 10. From the figure, It is found that variation in the values of heat absorption reduces energy transfer in the system by causing the temperature of the fluid to decrease. Therefore, the presence of heat sink in the boundary layer absorbs energy which influence the temperature of the fluid to decrease, and this corresponds with the observation in the figure.

Fig. 8. Concentration Profiles for different values of *Sc*

Fig. 9. Velocity Profiles for different values of *Da*

5. CONCLUSION

The effects of radiation, dissipation and chemical reaction on fluid flow, heat and mass transfer over an exponentially porous stretching surface in a porous medium was considered. The resulting governing equations are simplified and solved using fourth order Runge-Kutta method with shooting technique. The velocity distribution increases with an increase in the value of buoyancy forces but reduces as the porosity parameter rises. The fluid temperature profile increases with an increase in thermal radiation and thermal dissipation parameters while fluid temperature decreases with an increase in Prandtl number. Also, the concentration field decreases with an increase Schmidt number and chemical reaction term. The study is limited to Newtonian fluid. Hence, it can be extended to non-Newtonian fluid flow, turbulent and compressible flow.

COMPETING INTERESTS

Authors have declared that no competing interests exist.

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